

Composite Load Model Testing

Testing done by

Ran Xu at the Bonneville Power Administration

Tom Overbye and Komal Shetye at the University of Illinois

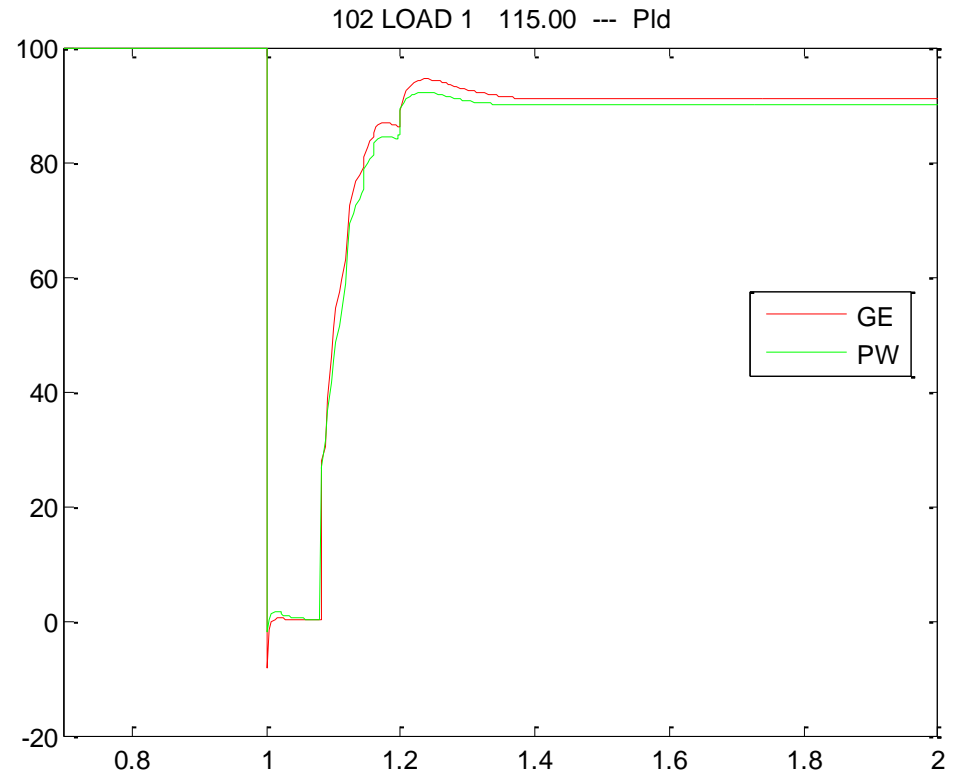
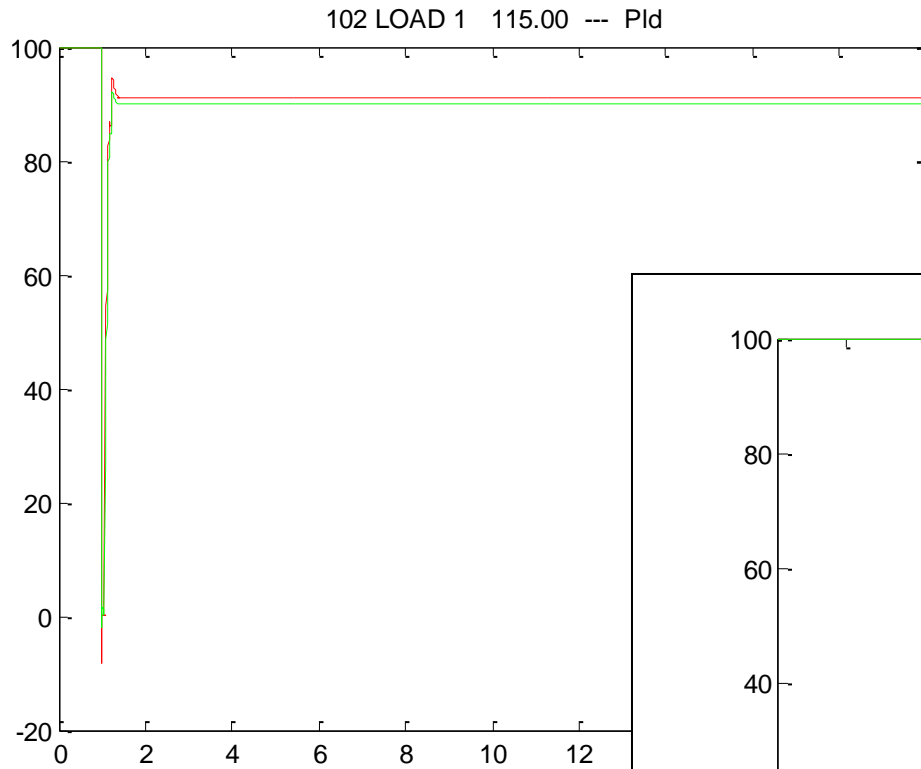
Song Wang at PacifiCorp (did PSSE runs for comparison)

October 2014

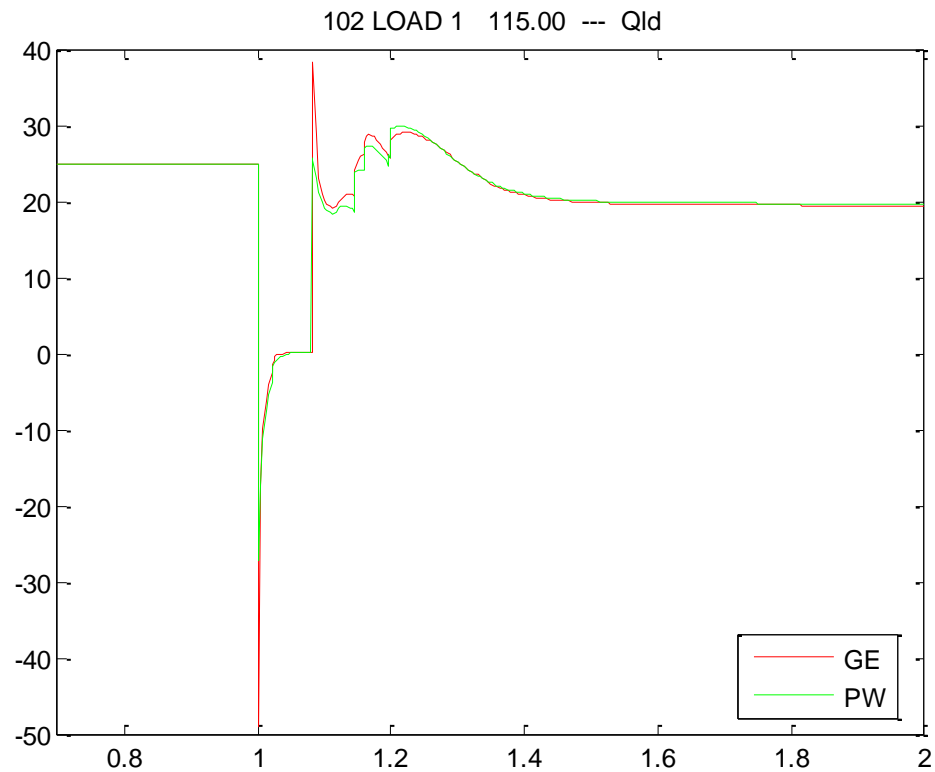
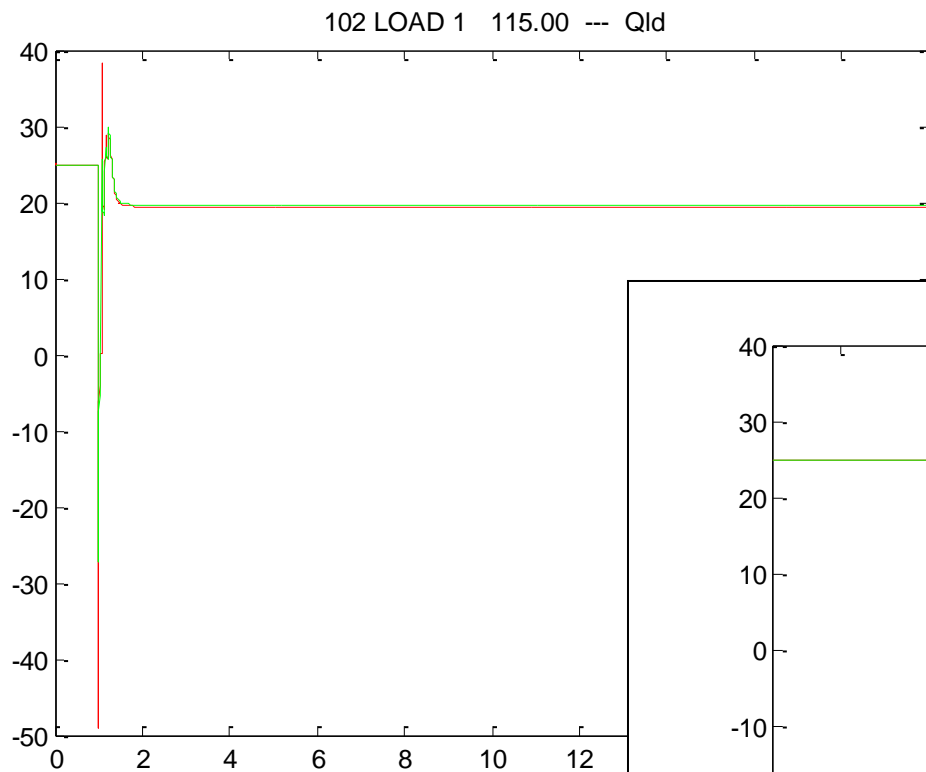
Benchmarking of CMPLDW

- Testing both “Phase 1” and “Phase 2” CMPLDW models
 - “Phase 1” means the CMPLDW without including the single-phase air-conditioner model
 - “Phase 2” means it includes the single-phase air-conditioner model with stalling
- This work focused on testing results in GE PSLF and PowerWorld Simulator
 - Results show they have largely the same response
- Small amount of work was done with PSSE results as well (Frequency results and Torques)

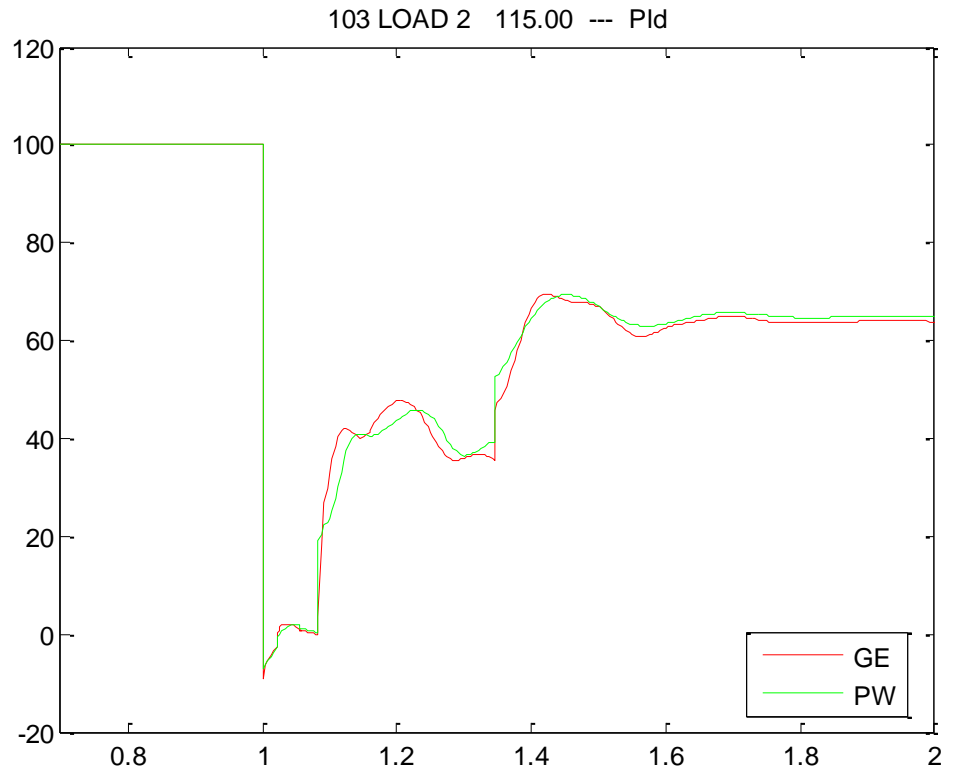
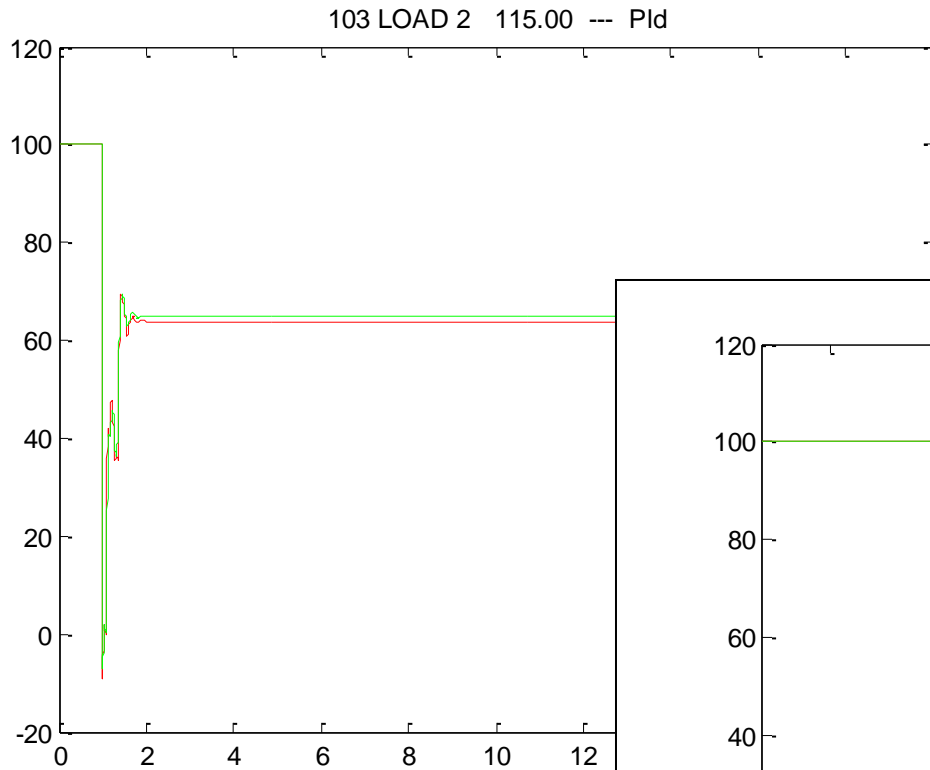
CMPLDW Total Load P with air-conditioner



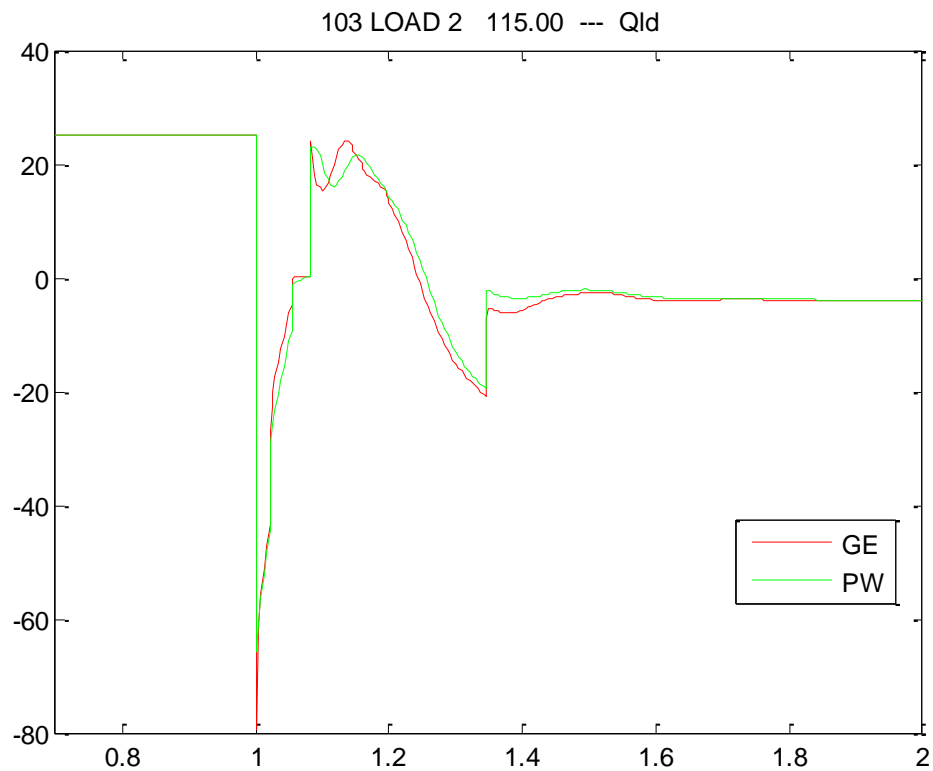
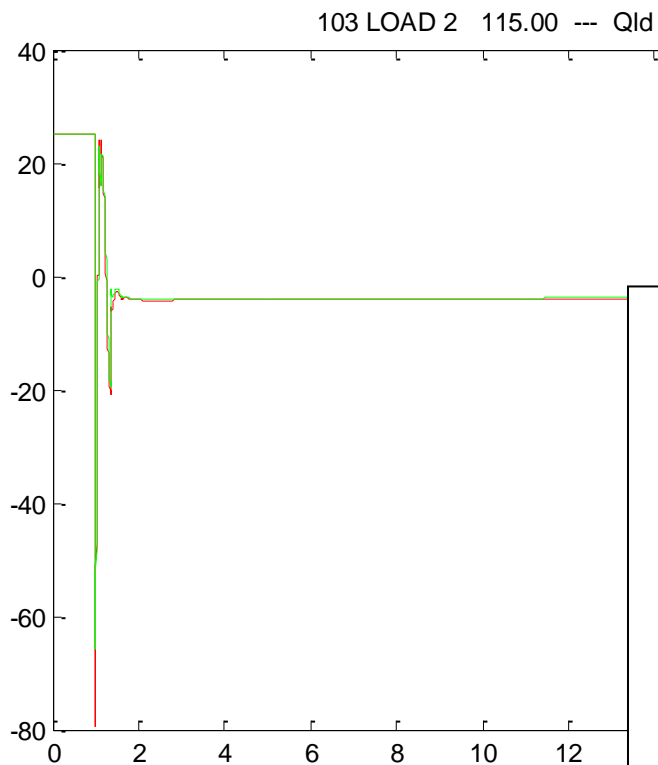
CMPLDW Total Load Q with air-conditioner



CMPLDW Total Load P without air-conditioner

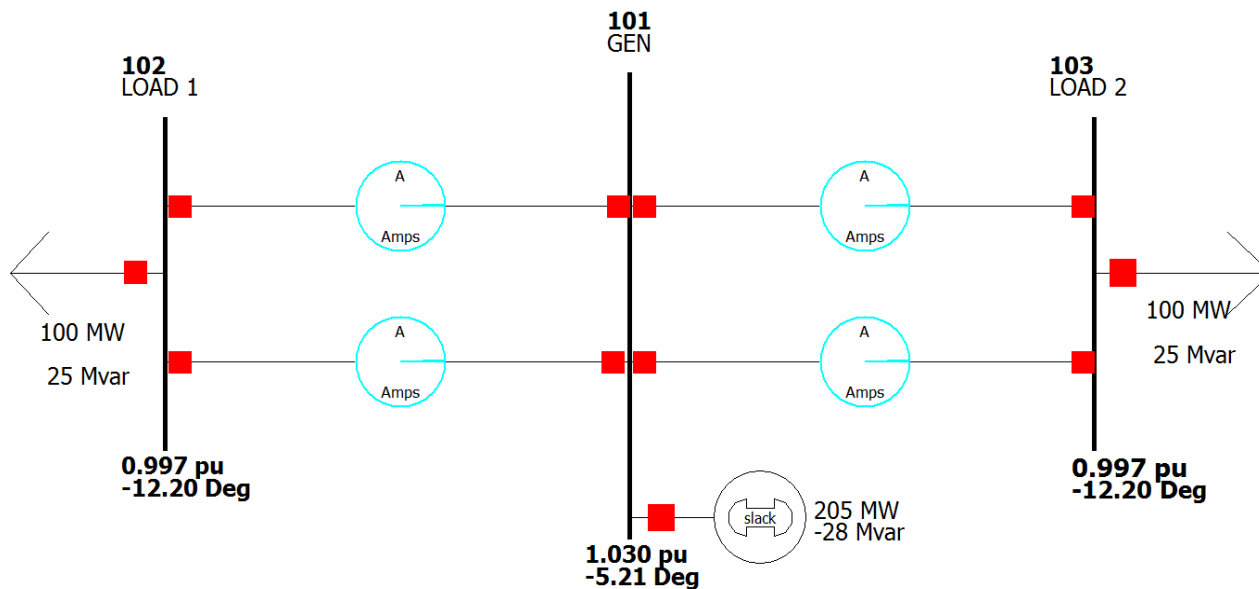


CMPLDW Total Load Q without air-conditioner



Test Simulation

- Three phase fault at bus 101 for 5 cycles (0.083333 seconds).
- Clear fault by opening one of each

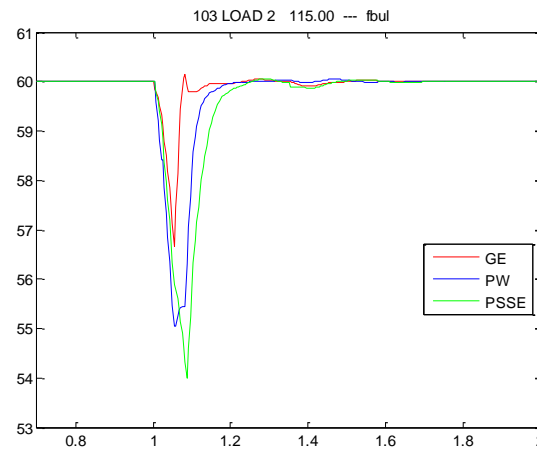
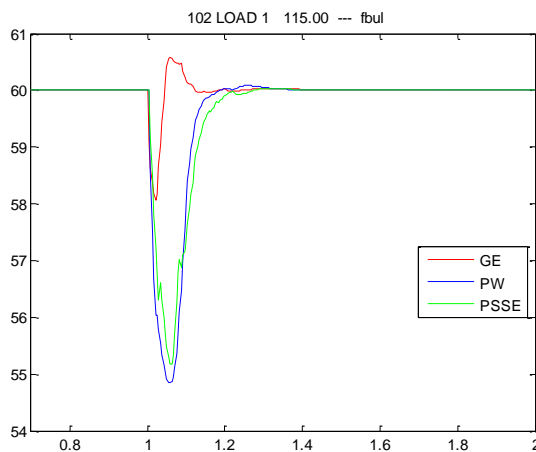


Findings

- Software Settings and Result Reporting Differences can cause confusion
- Communicated with PowerWorld staff and got some bugs fixed
- Have some open questions about appropriate way to model motors

Fault Impedance Might Matter

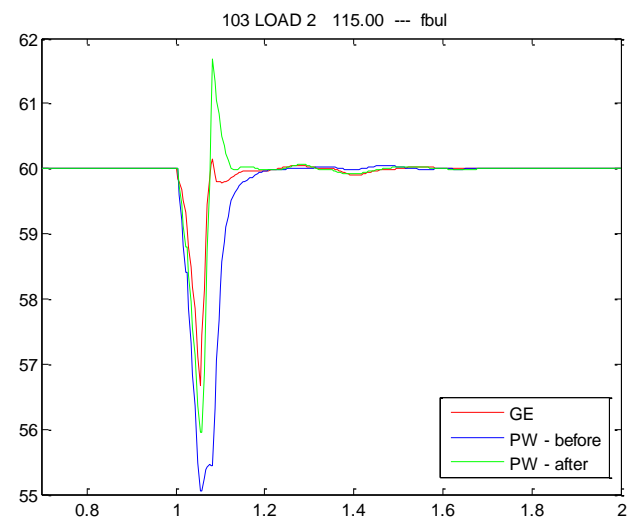
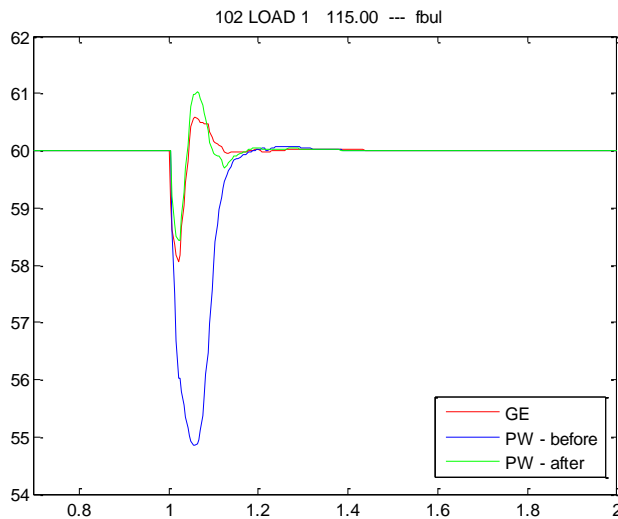
- Initial Frequency Results
 - PSLF was different. Frequency dip only to 58 Hz instead of 55 Hz



- Solely due to the default fault impedance

Fault Impedance Might Matter

- PowerWorld staff let us know that for a “solid” fault, a fault reactance of $1E-8$ is used
 - When fault reactance set to $1E-5$, results match those of PSLF –presumably that’s what is used



Why does fault impedance matter

- Artifact of this example case
 - Generator internal impedance $X_{dpp} = 0.2$ per unit, but $MVA_{Base} = 125,000$ MVA
 - On a system MVA_{Base} , that means
 - $X_{dpp}(\text{System}) = 0.2 * 100/125000 = 1.6E-4$
 - $1.6E-4$ about the same order as the $1E-5$ fault impedance, thus this fault impedance is too big for this particular example
 - In a real WECC case, this is not a concern, but can be on these little simple test cases.
- For remainder of testing a fault impedance of $1E-5$ was inserted into PowerWorld contingency

Variation of Fault Impedance



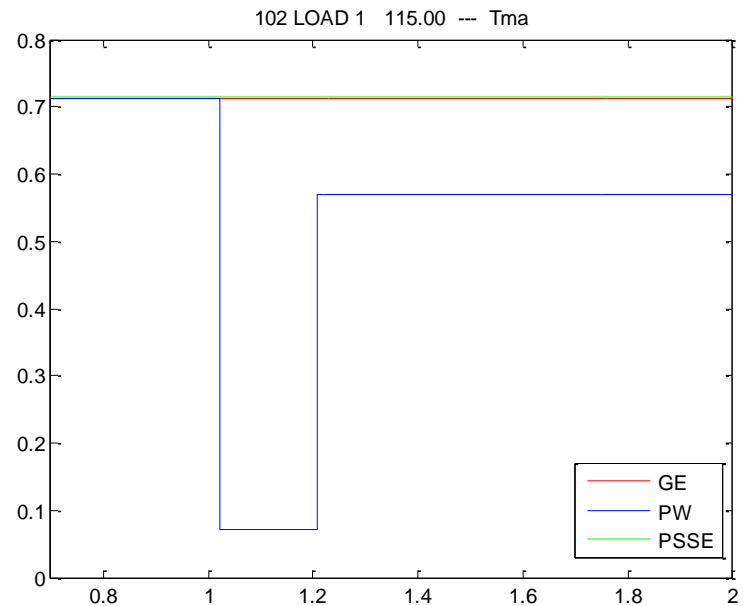
CMPLDW Motor Tripping

- For induction motors, CMPLDW allows “50% of motor to trip”
 - For a real motor, this makes no sense
 - CMPLDW is meant to model 100s or 1000s of motors though
 - This just means that half of them trip
- How does CMPLDW model motors
 - Models equations of only **ONE** motor
 - Then adds a scalar multiplier on the network boundary equations to scale the percentage of the load seen by the network
 - Essentially you can think of it as a variable “MVABase”
 - Question: How should we report motor torque?

How to report Motor Torque?

Per Unit or MWs

- Prior to July 15, 2014 PowerWorld would report torque in per unit based on the initial MVABase.
- Thus as percentage of motors were tripped, the torque would move
- PSSE and PSLF reported the internal torque of equations without the scalar
- All these simulations are correct
 - This is solely a reporting issue



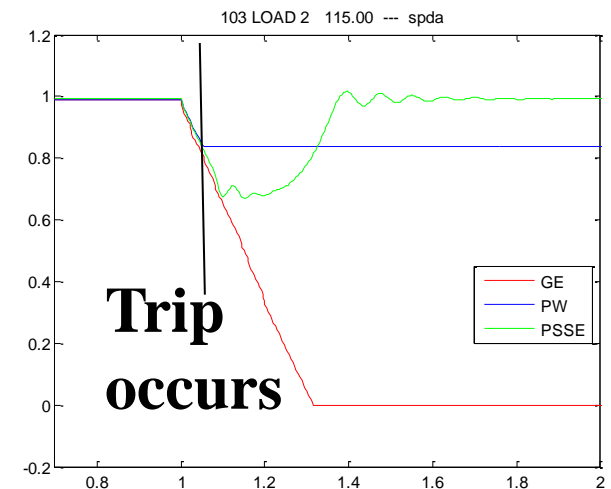
Changes to Simulator help with reporting

- Starting July 16, 2014, PowerWorld Simulator reports values scaled to MWs
- PowerWorld added extra “other fields” for the CMPLDW model to report for each motor (A, B, C, D)
 - Fraction not Tripped on Undervoltage
 - Present MVABase of motor
 - To get per unit then just take the MW values and divide by MVABase

$$T(pu) = T(MW) / MVABase$$

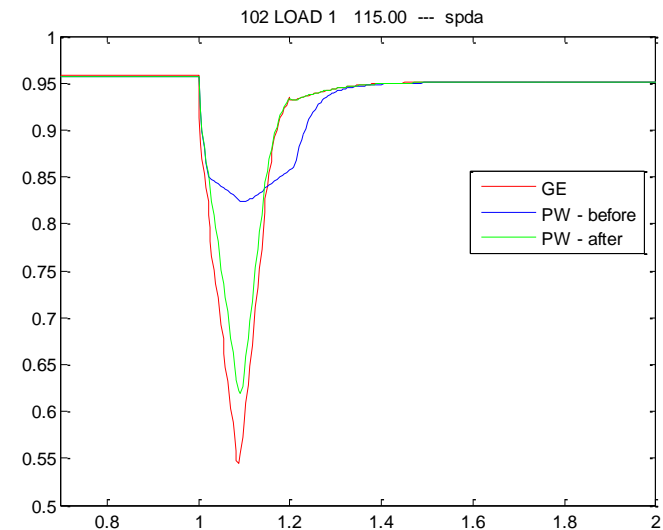
Speed Reporting after 100% Tripped

- CMPLDW allows motors to “reconnect” after they trip
 - This is just changing the scalar multiplier talked about on last slides
 - However, CMPLDW specifies that after 100% of the motor has tripped then it may NOT reconnect
 - PowerWorld Simulator simply quits integrating the equations associated with any out-of-service element which can not be reconnected
 - It truly doesn't matter at all



Bug Fixes: Motor Speed for percentage trip

- MOTORW allows under-voltage tripping, but only 100% tripping is permitted
- CMPLDW allows you to trip a percentage of the motor as we've discussed
- There was a bug when a percentage of the motor was tripped in the motor speed derivative calculation
 - Fixed in patch on Sept 19, 2014
 - A related bug existed when 100% of load was tripped as well which was fixed in Sept 23, 2014 patch

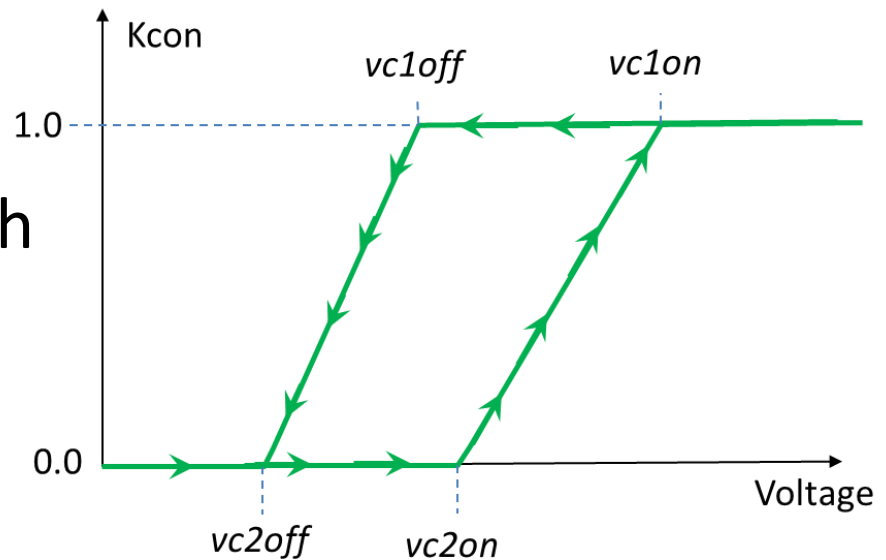


Single-Phase Air-Conditioner

Tvd delay on Contactor

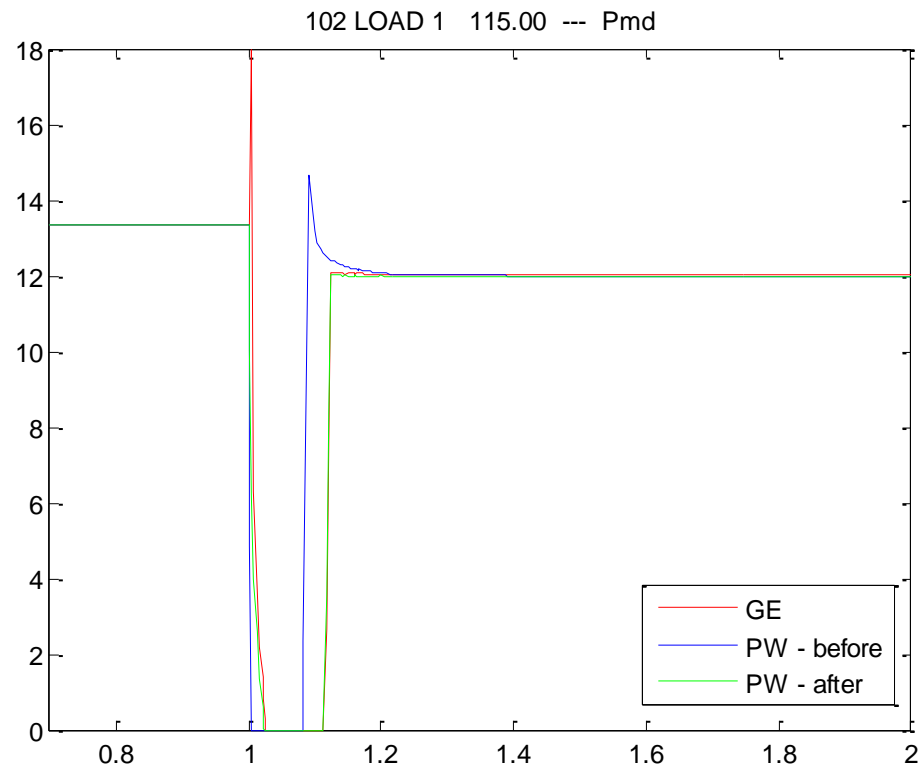
- Contactor Model

- The x-axis should be AFTER the measurement delay specified by Tvd
- PowerWorld Simulator was not properly using that delay
- This has been fixed in the Sept 19, 2014 patch



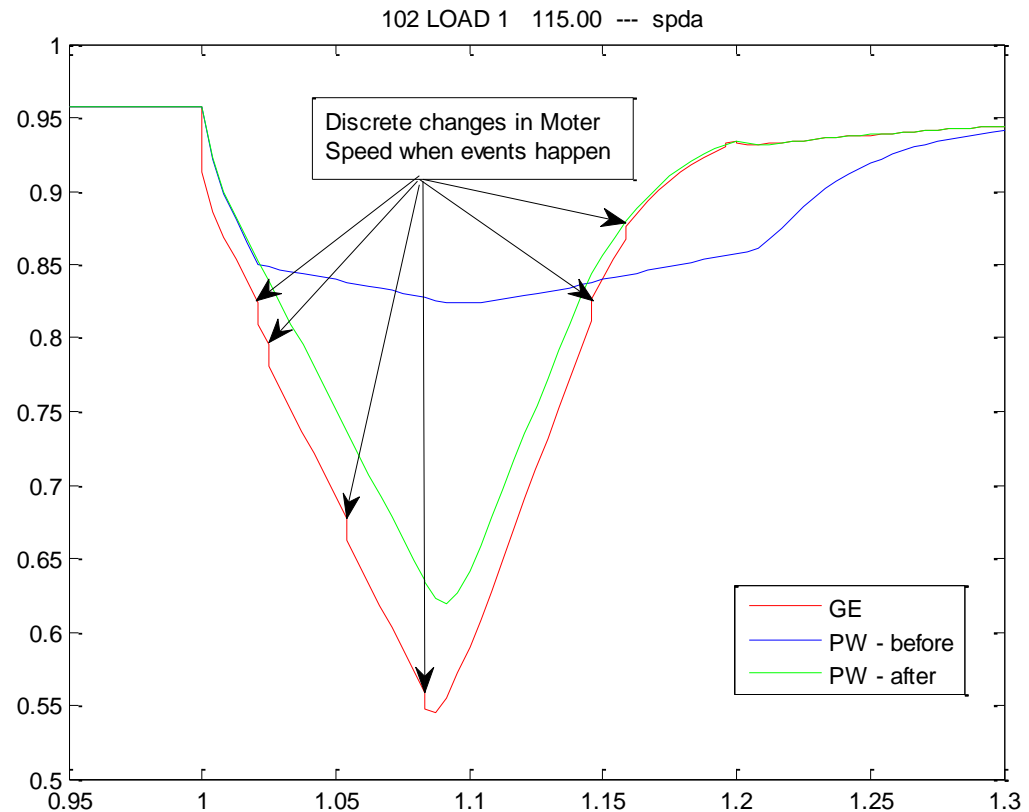
Bug Fixed in using measured voltage in contactor model

- $T_{vd} = 0.025$ in sample case
- See delay in green and red lines recovering equation to 0.025 seconds



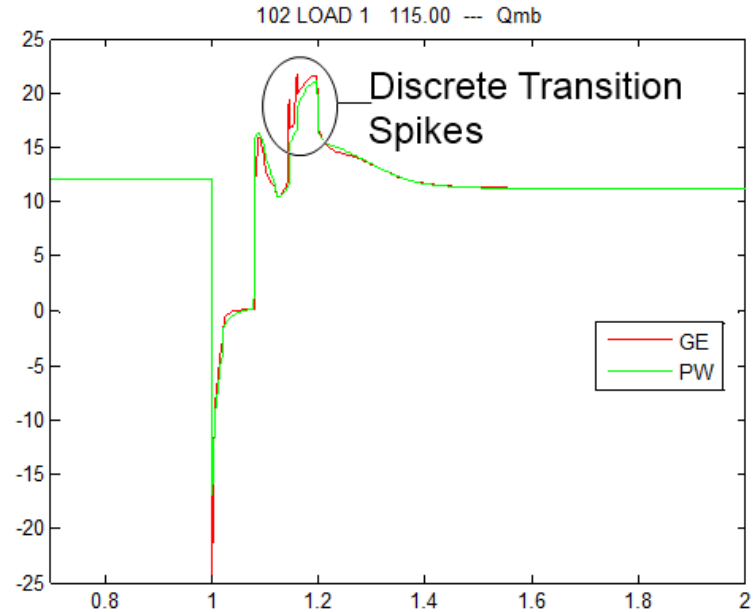
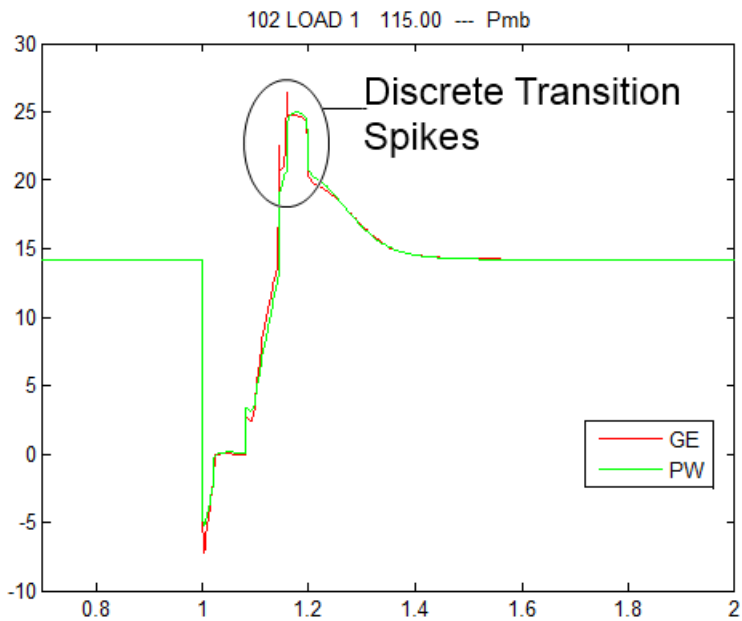
Discrete Changes in Induction Motor Speed

- Biggest remaining difference is the motor speed differences: What causes these?



Discrete Transition Spikes

- These spikes have little impact on the results, but one must be aware of them when comparing results.

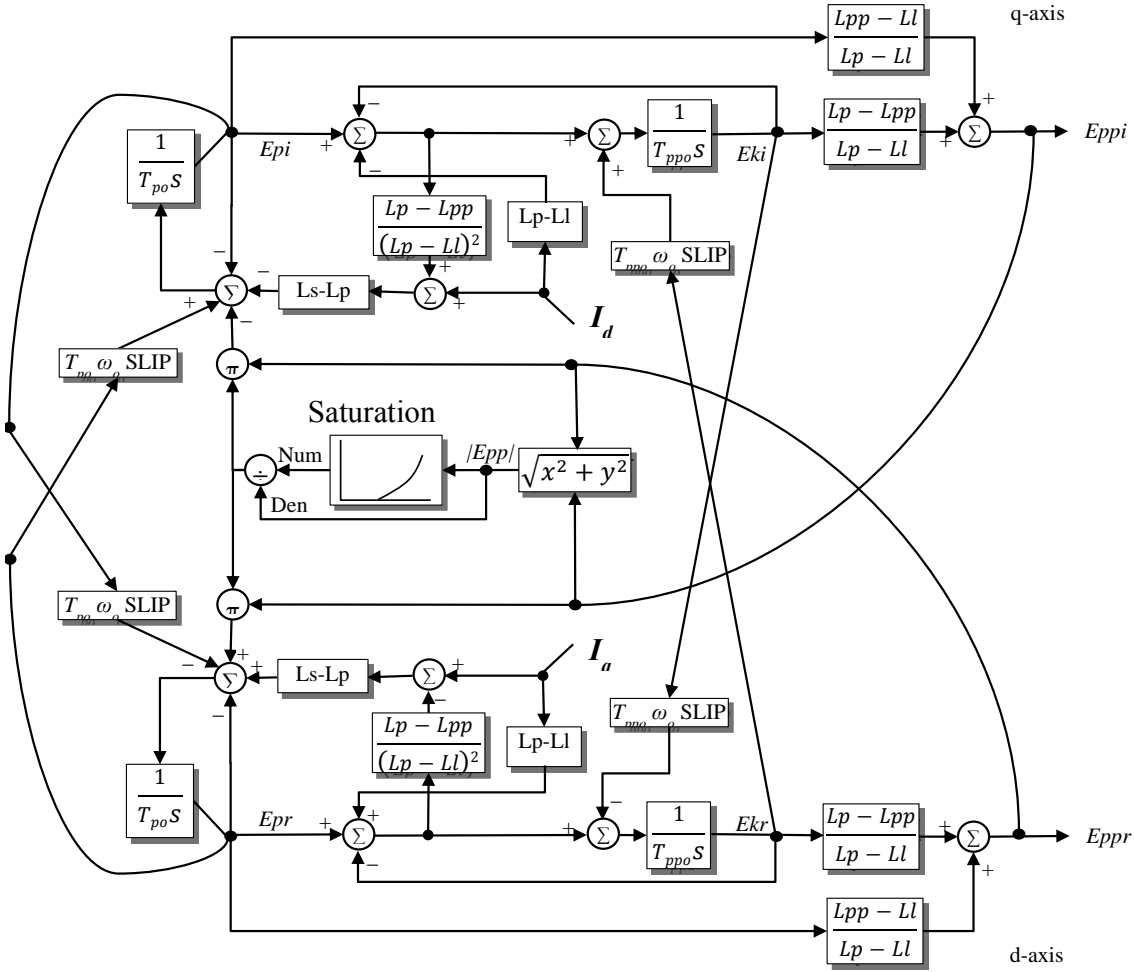


MOTORW difference with Induction Motor Models

- Induction motors can be represented by any of the following models
 - Load Models: CIM5, CIM6, CIMW
 - 7 Parameters: R_a , X_a , X_m , R_1 , X_1 , R_2 , X_2
 - Generator Model: MOTOR1, GENIND
 - 7 parameters: L_s , L_p , R_a , T_{po} , L_{pp} , T_{ppo} , L_I
 - Load Model: MOTORW
 - 6 parameters: L_s , L_p , R_a , T_{po} , L_{pp} , T_{ppo}
- There is an algebraic relationship between the 7 parameters in CIMx and MOTOR1, so they are identical models
- MOTORW leaves out the “ L_I ” term
- For a single-cage motor [($T_{ppo} = 0$) or ($L_{pp}=L_p$)] all these models are identical
- Historically MOTORW models had input data that represented single-cage motors only
 - Old WECC MOTORW model always used $T_{ppo} = 0$ and $L_{pp}=L_p=0.17$

Open
Question

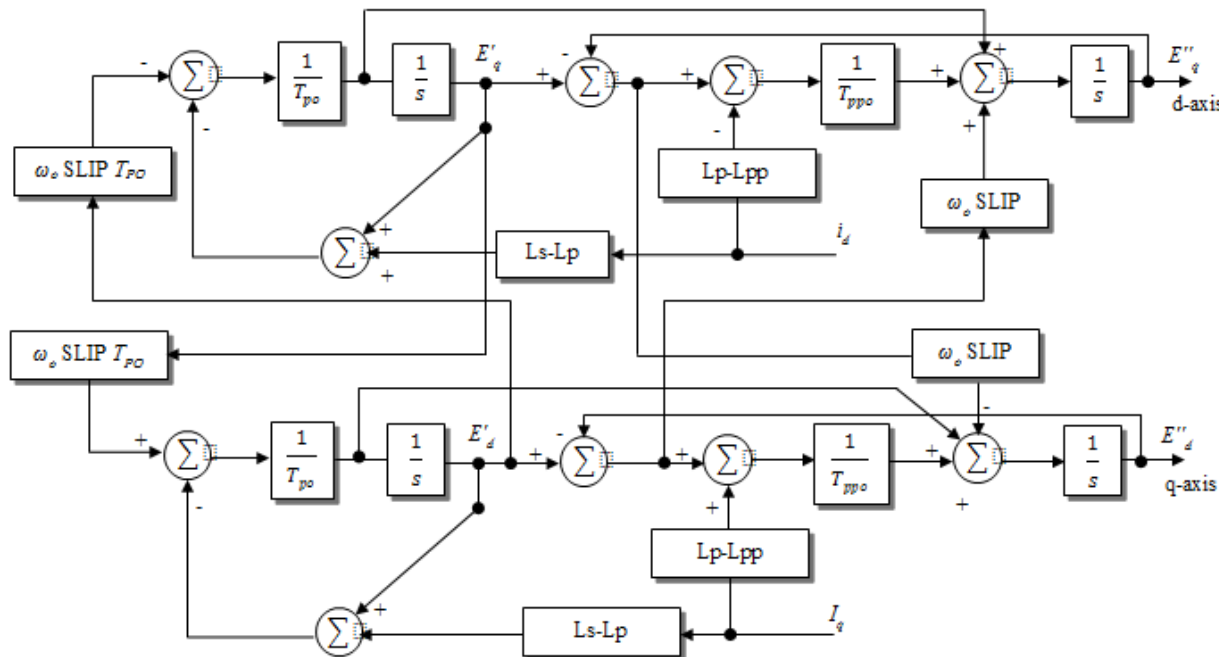
Standard Induction Motor Block Diagram



CIM5, CIM6, CIMW
and MOTOR1

MOTORW is slightly different

- With a bit of thinking, you can prove to yourself that these are the same if $L_{pp}=L_p$ and $T_{ppo} = 0$

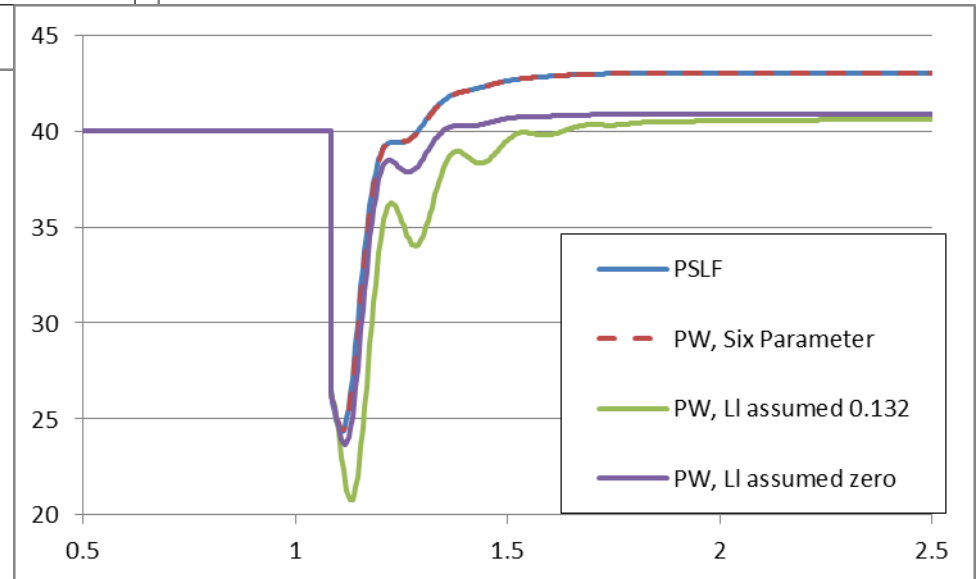
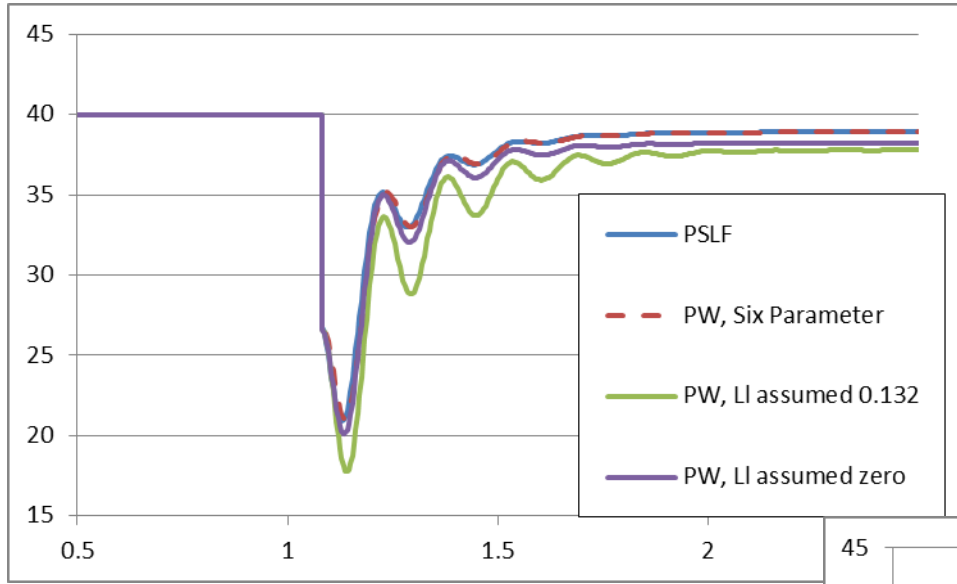


**CIM5, CIM6, CIMW
and MOTOR1**

Simulator Options

- Prior to July 17, 2014, PowerWorld Simulator assumed that the MOTORW model worked the same as CIM5 and assumed that
 - $Ll = 0.8 * Lpp$
- Models are different however.
 - We can not just assume something link “ $Ll=0$ ” or “ $Ll=Lpp$ ”, etc...
- Starting July 17, 2014 PowerWorld has added an option on how to treat MOTORW
 - Default is to change to the alternative induction motor block diagram used for MOTORW

CIMx will never match MOTORW for a Double-Cage Motor



Final Results

- The following slides show all the results for all the runs done

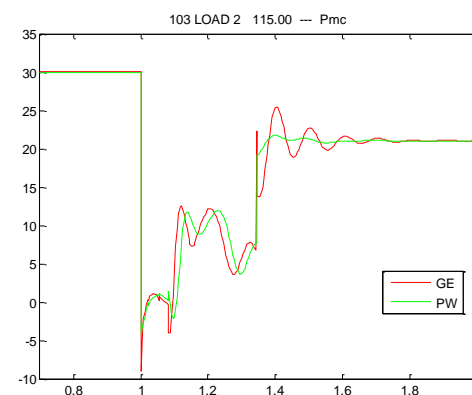
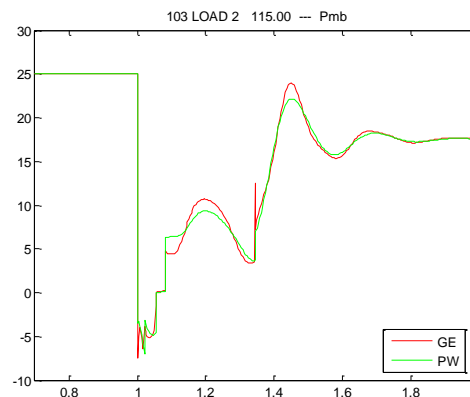
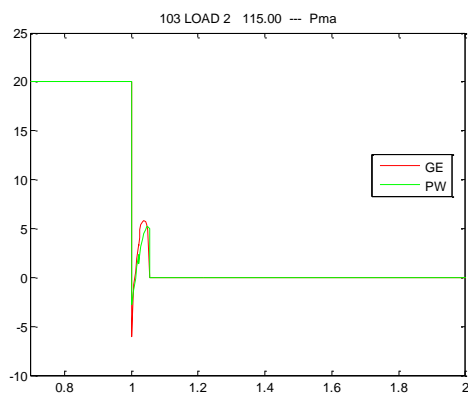
“Phase 1” Motor A, B, C MW and Mvar Results

Motor A

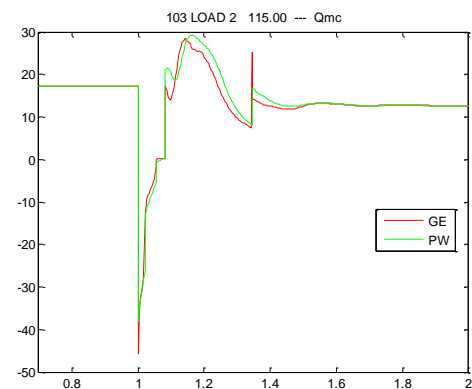
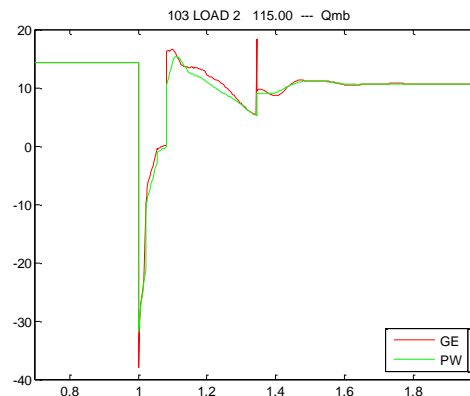
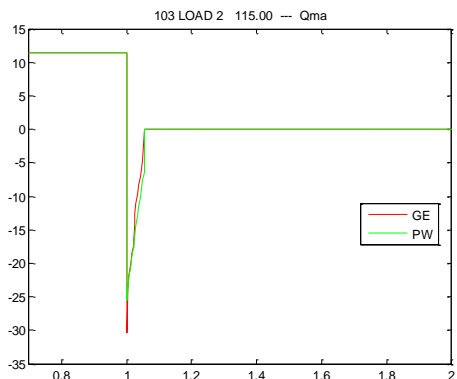
Motor B

Motor C

P [MW]



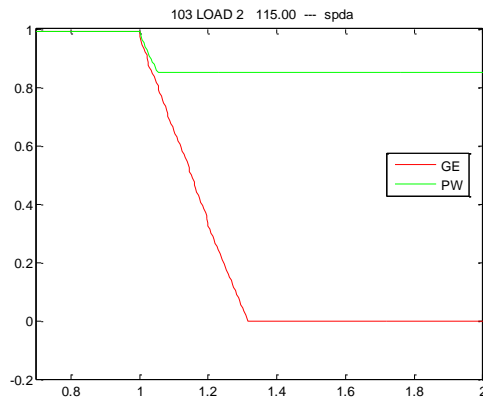
Q [Mvar]



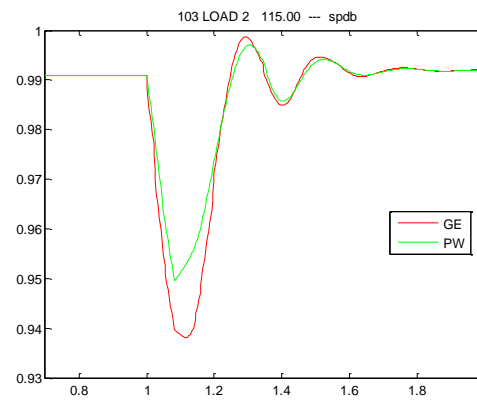
“Phase 1” Motor A, B, C

Motor Speed Results

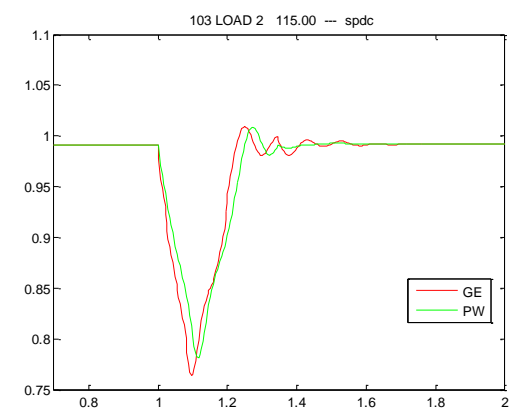
Motor A



Motor B



Motor C

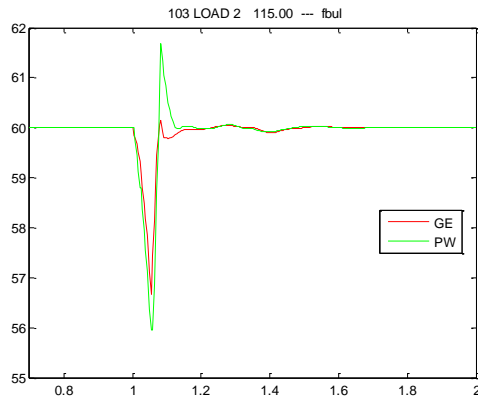


Speed

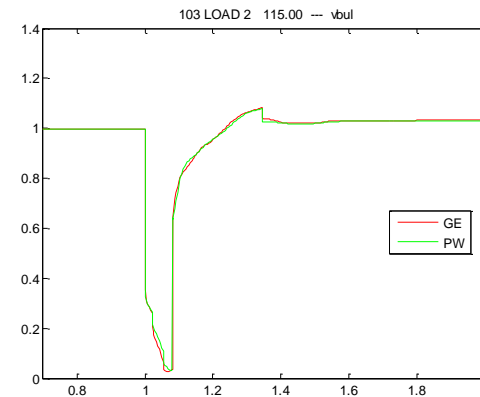
“Phase 1”

Distribution Equivalent Voltage

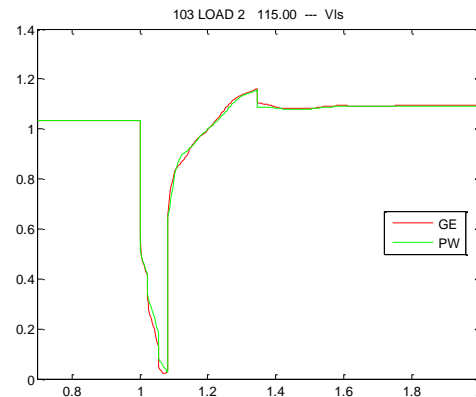
Frequency



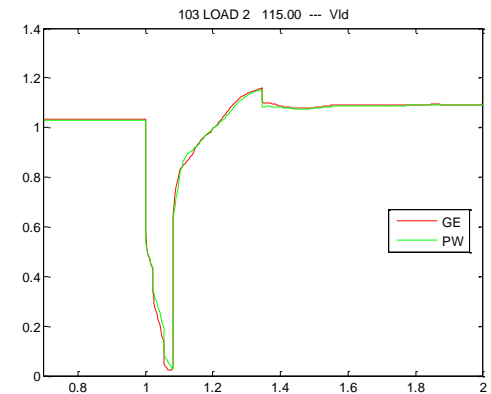
Voltage at Transmission



Voltage Low Side

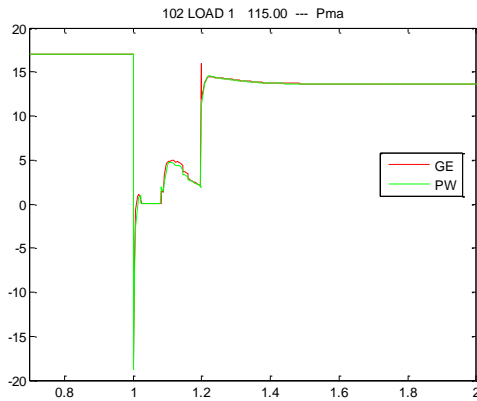


Voltage at Load Bus

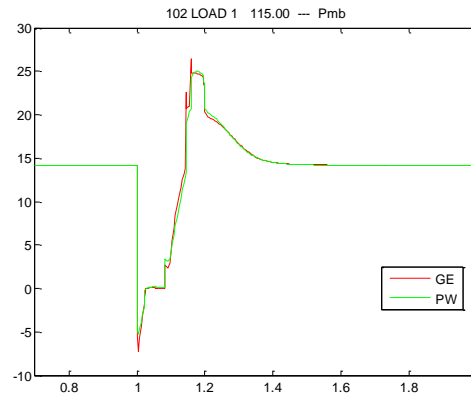


“Phase 2” Motor A, B, C MW and Mvar Results

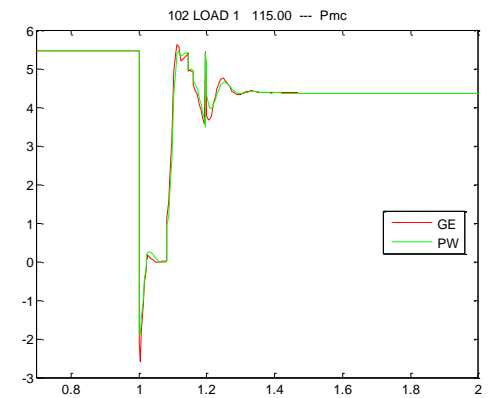
Motor A



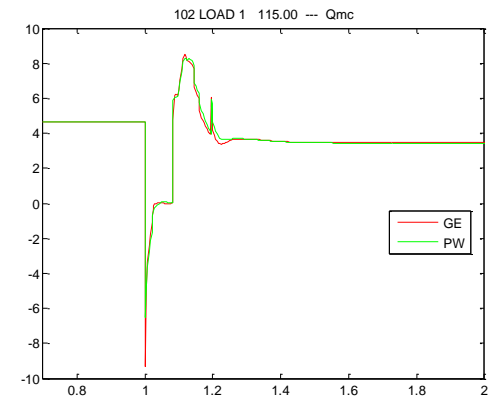
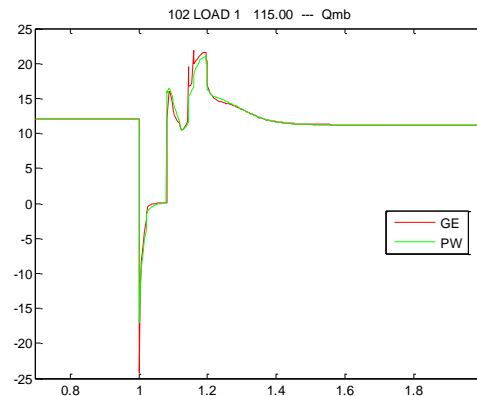
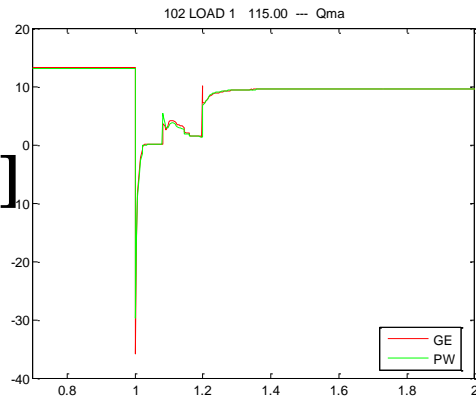
Motor B



Motor C

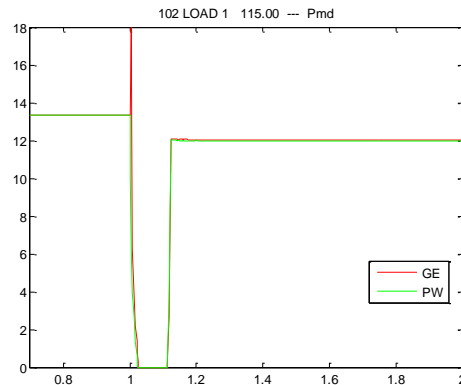


Q [Mvar]

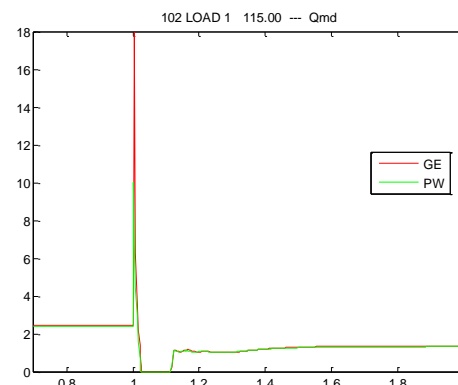


“Phase 2” Motor D Power Result single-phase air-conditioner

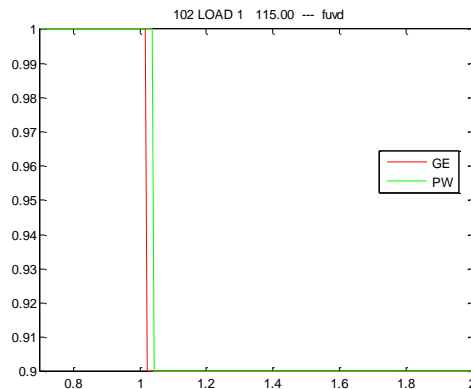
P [MW]



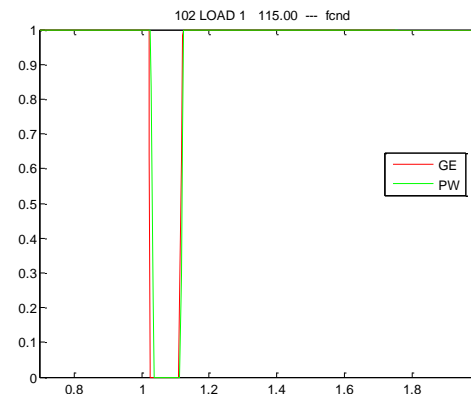
Q [Mvar]



Under Voltage Multiplier



Contactors Multiplier



“Phase 2” Motor A, B, C

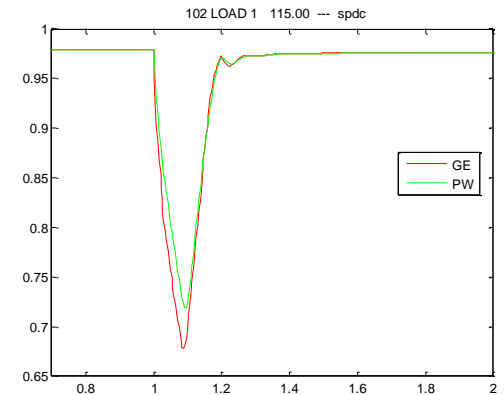
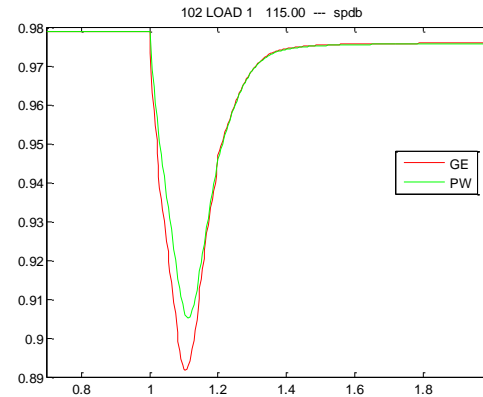
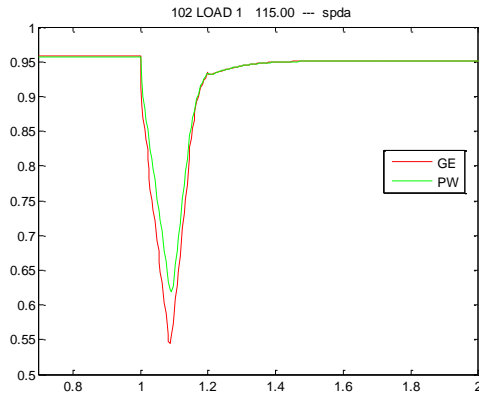
Motor Speed Results

Motor A

Motor B

Motor C

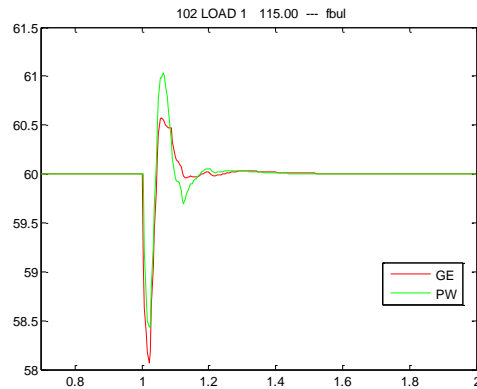
Speed



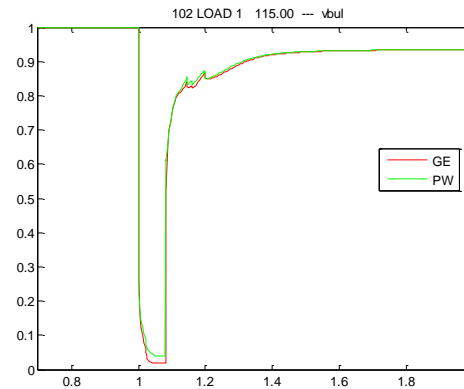
“Phase 2”

Distribution Equivalent Voltage

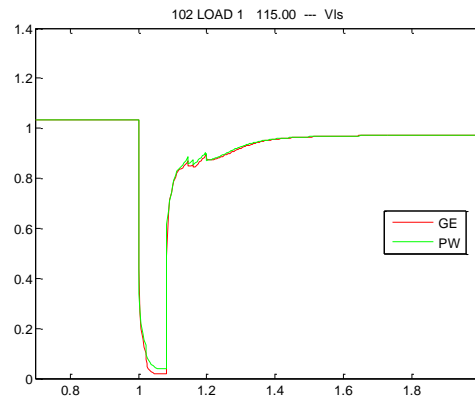
Frequency



Voltage at Transmission



Voltage Low Side



Voltage at Load Bus

